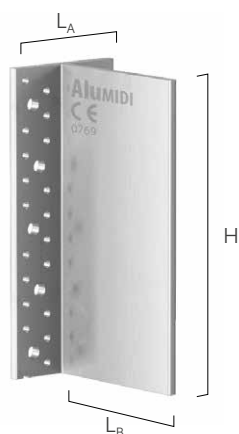


ALUMIDI HT

CONCEALED BRACKET WITH AND WITHOUT HOLES

- Large load capacity. Version without holes to be used with SBD-HT self-drilling dowels and with holes to be used with STA smooth dowels
- Strengths calculated in all directions: vertical, horizontal and axial. They can be used in inclined joints
- Optimal hole spacing both for timber and reinforced concrete joints

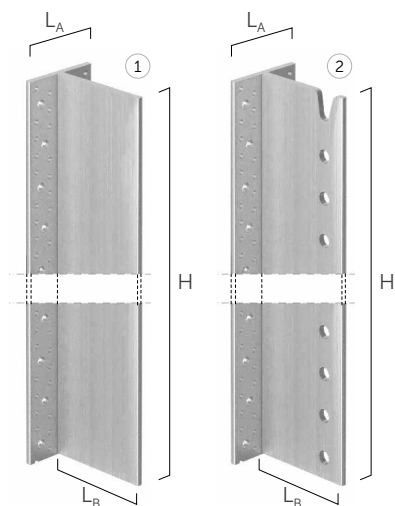


ALUMIDI HT WITHOUT HOLES

CODE	H [mm]	L _A [mm]	L _B [mm]	pcs
ALUMIDIHT80	80	80	109	25
ALUMIDIHT120	120	80	109	25
ALUMIDIHT160	160	80	109	25
ALUMIDIHT200	200	80	109	15
ALUMIDIHT240	240	80	109	15
ALUMIDIHT2200	2200	80	109	1

ALUMIDI WITH HOLES

CODE	H [mm]	L _A [mm]	L _B [mm]	pcs
ALUMIDI120L	120	80	109	25
ALUMIDI160L	160	80	109	25
ALUMIDI200L	200	80	109	15
ALUMIDI240L	240	80	109	15
ALUMIDI280L	280	80	109	15
ALUMIDI320L	320	80	109	8
ALUMIDI360L	360	80	109	8



ALUMAXI WITH AND WITHOUT HOLES

CODE		H [mm]	L _A [mm]	L _B [mm]	pcs
ALUMAXI2176	①	2176	130	172	1
ALUMAXI2176L	②	2176	130	172	1

FASTENERS

SBD-HT | SELF-DRILLING DOWEL

d ₁ [mm]	CODE	L [mm]	b ₂ [mm]	b ₁ [mm]	pcs
7,5 TX 40	SBD75115H	115	10	15	50
	SBD75135H	135	10	15	50
	SBD75155H	155	20	15	50

STA | SMOOTH DOWEL

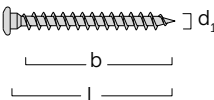
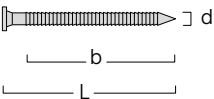
d ₁ [mm]	CODE	L [mm]	steel	pcs
12	STA12120B	120	S235	100
	STA12140B	140	S235	100
	STA12160B	160	S235	100
16	STA16160B	160	S355	50
	STA16180B	180	S355	50
	STA16200B	200	S355	50

LBA-HT | ANKER NAIL

d ₁ [mm]	CODE	L [mm]	b [mm]	pcs
4	HT4060	60	50	250
6	LBA6100	100	80	250

SBL | ROUND-HEAD SCREW AND FLAT UNDERHEAD

d ₁ [mm]	CODE	L [mm]	b [mm]	pcs
5 TX 20	SBL560	60	56	200
7 TX 30	LBS780	80	75	100



STRUCTURAL VALUES

TIMBER-TO-TIMBER JOINT | F_v



ALUMIDI HT without holes with SBD-HT self-drilling dowels

	SECONDARY BEAM			MAIN BEAM				
ALUMIDI HT				FASTENING THROUGH NAILS		FASTENING THROUGH SCREWS		
	H [mm]	b _j [mm]	h _j [mm]	SBD-HT dowels ⁽¹⁾	LBA-HT nails	R _{V,k}	SBL screws	R _{V,k}
				Ø7,5 [pcs Ø x L]	Ø4 x 60 [pcs]	[kN]	Ø5 x 60 [pcs]	[kN]
80	120	120		3 - Ø7,5 x 115	14	10,9	14	13,4
120	120	160		4 - Ø7,5 x 115	22	19,7	22	24,6
160	120	200		5 - Ø7,5 x 115	30	29,6	30	35,3
200	120	240		7 - Ø7,5 x 115	38	42,5	38	51,6
240	120	280		9 - Ø7,5 x 115	46	54,6	46	66,5
280 ^(*)	140	320		10 - Ø7,5 x 135	54	71,8	54	85,0
320 ^(*)	140	360		11 - Ø7,5 x 135	62	84,9	62	99,9
360 ^(*)	160	400		12 - Ø7,5 x 155	70	103,6	70	119,9
400 ^(*)	160	440		13 - Ø7,5 x 155	78	116,3	78	130,7
440 ^(*)	160	480		14 - Ø7,5 x 155	86	134,5	86	145,6

ALUMIDI with holes with STA dowels

	SECONDARY BEAM			MAIN BEAM			
ALUMIDI HT				FASTENING THROUGH NAILS		FASTENING THROUGH SCREWS	
			STA dowels ⁽²⁾	LBA-HT nails	R _{V,k}	SBL screws	R _{V,k}
	H	b _J	h _J	Ø12	Ø4 x 60	Ø5 x 60	
[mm]	[mm]	[mm]	[pcs Ø x L]	[pcs]	[kN]	[pcs]	[kN]
120	120	160	3 - Ø12 x 120	22	23,0	22	25,8
160	120	200	4 - Ø12 x 120	30	34,5	30	40,6
200	120	240	5 - Ø12 x 120	38	46,5	38	54,8
240	120	280	6 - Ø12 x 120	46	60,9	46	68,4
280	140	320	7 - Ø12 x 140	54	77,2	54	87,0
320	140	360	8 - Ø12 x 140	62	93,2	62	102,4
360	160	400	9 - Ø12 x 160	70	114,3	70	124,7
400 ^(*)	160	440	10 - Ø12 x 160	78	127,3	78	141,0
440 ^(*)	160	480	11 - Ø12 x 160	86	144,6	86	154,9

NOTES

(*) Dimension obtainable from ALUMIDIHT2200.

TIMBER-TO-TIMBER | F_v

(1) SBD-HT self-drilling dowels Ø7,5: $M_{y,k} = 42000 \text{ Nmm}$.

(2) STA smooth dowels Ø12: $M_{y,k} = 69100 \text{ Nmm}$.

General calculation principles, see page 8.

STRUCTURAL VALUES

TIMBER-TO-TIMBER JOINT | F_{lat}



ALUMIDI HT without holes with SBD-HT self-drilling dowels | ALUMIDI with holes with STA dowels

ALUMIDI HT	SECONDARY BEAM ⁽¹⁾		MAIN BEAM ⁽²⁾		$R_{lat,k,alu}$ [kN]	$R_{lat,k,beam}^{(3)}$ [kN]
	b_j [mm]	h_j [mm]	LBA-HT nails / SBL screws $\varnothing 4 \times 60$ / $\varnothing 5 \times 60$ [pcs]			
80	120	120	≥ 10		3,6	9,0
120	120	160	≥ 14		5,4	12,0
160	120	200	≥ 18		7,2	15,0
200	120	240	≥ 22		9,1	18,0
240	120	280	≥ 26		10,9	21,0
280 ^(*)	140	320	≥ 30		12,7	28,1
320 ^(*)	140	360	≥ 34		14,5	31,6
360 ^(*)	160	400	≥ 38		16,3	40,1
400 ^(*)	160	440	≥ 42		18,1	44,1
440 ^(*)	160	480	≥ 46		19,9	48,1

TIMBER-TO-TIMBER JOINT | F_{ax}



ALUMIDI HT without holes with SBD-HT self-drilling dowels

ALUMIDI HT	SECONDARY BEAM			MAIN BEAM			
	b_j [mm]	h_j [mm]	SBD-HT dowels $\varnothing 7,5$ [pcs $\varnothing \times L$]	FASTENING THROUGH NAILS LBA-HT nails $\varnothing 4 \times 60$ [pcs]	$R_{ax,k}^{(3)}$ [kN]	FASTENING THROUGH SCREWS SBL screws $\varnothing 5 \times 60$ [pcs]	$R_{ax,k}^{(3)}$ [kN]
80	120	120	3 - $\varnothing 7,5 \times 115$	14	11,3	14	23,9
120	120	160	4 - $\varnothing 7,5 \times 115$	22	17,8	22	37,5
160	120	200	5 - $\varnothing 7,5 \times 115$	30	24,3	30	51,2
200	120	240	7 - $\varnothing 7,5 \times 115$	38	30,8	38	64,8
240	120	280	9 - $\varnothing 7,5 \times 115$	46	37,3	46	78,4
280	140	320	10 - $\varnothing 7,5 \times 135$	54	43,7	54	92,1
320	140	360	11 - $\varnothing 7,5 \times 135$	62	50,2	62	105,7
360	160	400	12 - $\varnothing 7,5 \times 155$	70	56,7	70	119,4
400 ^(*)	160	440	13 - $\varnothing 7,5 \times 155$	78	63,2	78	133,0
440 ^(*)	160	480	14 - $\varnothing 7,5 \times 155$	86	69,7	86	146,6

NOTES

^(*) Dimension obtainable from ALUMIDIHT2200.

TIMBER-TO-TIMBER | F_{lat} | F_{ax}

⁽¹⁾ The strength values are valid for both SBD-HT $\varnothing 7,5$ self-drilling dowels and STA $\varnothing 12$ dowels.

⁽²⁾ The strength values are valid for both LBA-HT $\varnothing 4$ nails and for SBL $\varnothing 5$ screws.

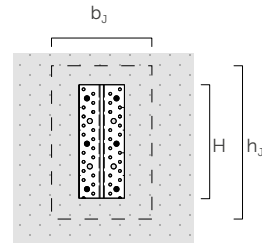
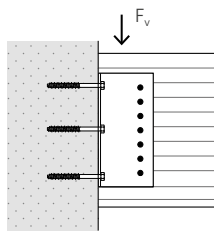
⁽³⁾ The strength values have been calculated for GL24h glulam.

General calculation principles, see page 8.

STRUCTURAL VALUES

TIMBER-TO-CONCRETE JOINT | F_v

CHEMICAL ANCHOR



ALUMIDI HT without holes with SBD-HT self-drilling dowels

	SECONDARY BEAM TIMBER				MAIN BEAM uncracked concrete	
ALUMIDI HT				SBD-HT dowels	SKR-CE anchor	
H [mm]	b _j [mm]	h _j [mm]	Ø7,5 [pcs Ø x L]	R _{V,k timber} [kN]	Ø10 x 80 [pcs]	R _{V,d concrete} [kN]
80	120	120	2 - Ø7,5 x 115	16,6	2	6,1
120	120	160	3 - Ø7,5 x 115	24,9	4	10,2
160	120	200	4 - Ø7,5 x 115	33,2	4	12,9
200	120	240	5 - Ø7,5 x 115	41,6	6	17,4
240	120	280	6 - Ø7,5 x 115	49,9	6	19,8
280(*)	140	320	6 - Ø7,5 x 135	55,1	8	24,3
320(*)	140	360	7 - Ø7,5 x 135	64,3	8	26,5
360(*)	160	400	7 - Ø7,5 x 155	71,1	10	31,1
400(*)	160	440	8 - Ø7,5 x 155	81,2	10	33,1
440(*)	160	480	9 - Ø7,5 x 155	91,4	12	38,8

ALUMIDI with holes with STA dowels

	SECONDARY BEAM TIMBER				MAIN BEAM uncracked concrete	
ALUMIDI HT				STA dowels	SKR-CE anchor	
H [mm]	b _j [mm]	h _j [mm]	Ø12 [pcs Ø x L]	R _{V,k timber} [kN]	Ø10 x 80 [pcs]	R _{V,d concrete} [kN]
120	120	160	3 - Ø12 x 120	35,5	4	10,2
160	120	200	4 - Ø12 x 120	47,3	4	12,9
200	120	240	5 - Ø12 x 120	59,1	6	17,4
240	120	280	6 - Ø12 x 120	70,9	6	19,8
280(*)	140	320	7 - Ø12 x 140	91,0	8	24,3
320(*)	140	360	8 - Ø12 x 140	104,0	8	26,5
360(*)	160	400	9 - Ø12 x 160	128,4	10	31,1
400(*)	160	440	10 - Ø12 x 160	142,7	10	33,1
440(*)	160	480	11 - Ø12 x 160	157,0	12	38,8

NOTES

(*) Dimension obtainable from ALUMIDIHT2200.

TIMBER-TO-CONCRETE

- Install the SKR-CE screw anchors two at a time, starting from the top, dowelling alternate rows.

General calculation principles, see page 8.

STRUCTURAL VALUES

TIMBER-TO-CONCRETE JOINT | F_v

CHEMICAL ANCHOR



ALUMIDI HT without holes with SBD-HT self-drilling dowels

	SECONDARY BEAM TIMBER				MAIN BEAM uncracked concrete	
ALUMIDI HT			SBD-HT dowels		V-NEX anchor ⁽¹⁾	
H [mm]	b _j [mm]	h _j [mm]	Ø7,5 [pcs Ø x L]	R _{v,k} timber [kN]	Ø8 x 110 [pcs]	R _{v,d} concrete [kN]
80	120	120	3 - Ø7,5 x 115	24,9	2	8,8
120	120	160	4 - Ø7,5 x 115	33,2	4	15,4
160	120	200	5 - Ø7,5 x 115	41,6	4	22,1
200	120	240	7 - Ø7,5 x 115	58,2	6	30,7
240	120	280	8 - Ø7,5 x 115	66,5	6	37,0
280(*)	140	320	10 - Ø7,5 x 135	91,9	8	48,7
320(*)	140	360	11 - Ø7,5 x 135	101,1	8	55,6
360(*)	160	400	12 - Ø7,5 x 155	121,9	10	64,4
400(*)	160	440	13 - Ø7,5 x 155	132,0	10	66,4
440(*)	160	480	14 - Ø7,5 x 155	142,2	12	80,0

ALUMIDI with holes with STA dowels

	SECONDARY BEAM TIMBER				MAIN BEAM uncracked concrete	
ALUMIDI HT			STA dowels		V-NEX anchor ⁽¹⁾	
H [mm]	b _j [mm]	h _j [mm]	Ø12 [pcs Ø x L]	R _{v,k} timber [kN]	Ø8 x 110 [pcs]	R _{v,d} concrete [kN]
120	120	160	3 - Ø12 x 120	35,5	4	15,4
160	120	200	4 - Ø12 x 120	47,3	4	22,1
200	120	240	5 - Ø12 x 120	59,1	6	30,7
240	120	280	6 - Ø12 x 120	70,9	6	37,0
280(*)	140	320	7 - Ø12 x 140	91,0	8	48,7
320(*)	140	360	8 - Ø12 x 140	104,0	8	55,6
360(*)	160	400	9 - Ø12 x 160	128,4	10	64,4
400(*)	160	440	10 - Ø12 x 160	142,7	10	66,4
440(*)	160	480	11 - Ø12 x 160	157,0	12	80,0

NOTES

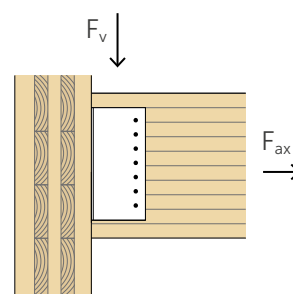
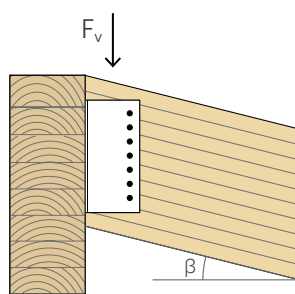
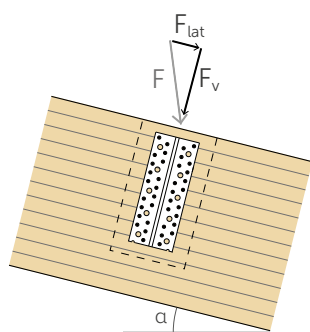
(*) Dimension obtainable from ALUMIDIHT2200.

TIMBER-TO-CONCRETE

⁽¹⁾ Chemical anchor V-NEX according to ETA-20/0363 with threaded rods (type INA) of minimum steel class 5.8 with h_{ef} = 93 mm: Install the anchors two at a time, starting from the top, dowelling alternate rows.

General calculation principles, see page 8.

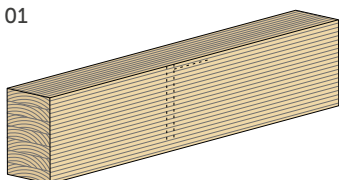
APPLICATION EXAMPLES



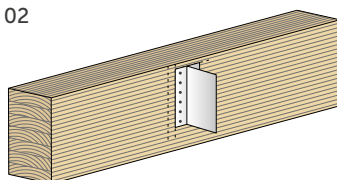
ASSEMBLY



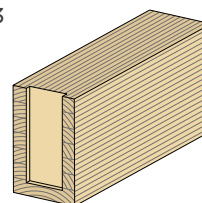
01



02

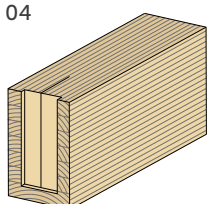


03

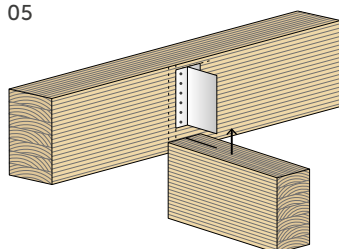


ALUMIDI HT WITHOUT HOLES

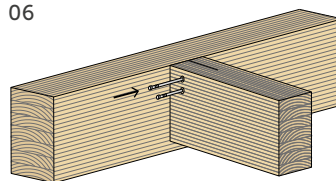
04



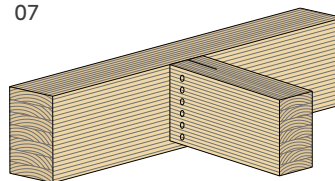
05



06

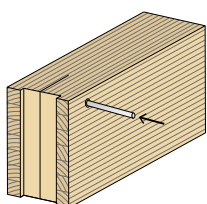


07

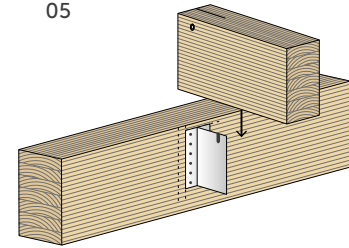


ALUMIDI HT WITHOUT HOLES WITH UPPER COUNTERSINK

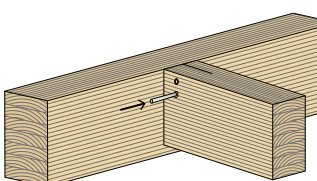
04



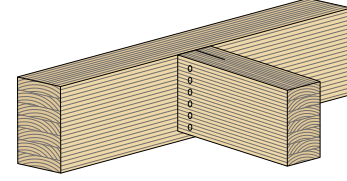
05



06

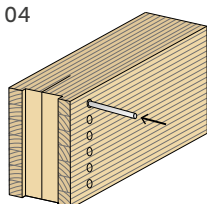


07

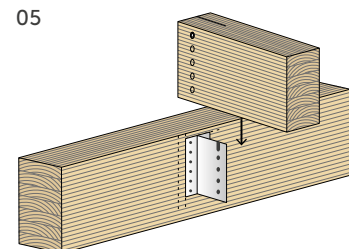


ALUMIDI WITH HOLES

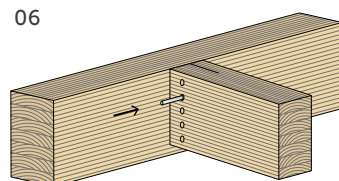
04



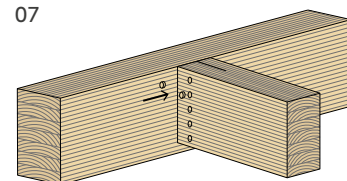
05



06



07



GENERAL PRINCIPLES

- Resistance values for the fastening system are valid for the calculation examples shown in the table.
- The calculation process used a timber characteristic density of $\rho_k = 385 \text{ kg/m}^3$ and C20/25 concrete with a thin reinforcing layer, where edge-distance is not a limiting factor.
- The coefficients k_{mod} and γ_M should be taken according to the current regulations used for the calculation.
- Dimensioning and verification of timber and concrete elements must be carried out separately.
- In case of combined loading the following verification shall be satisfied:

$$\left(\frac{F_{v,d}}{R_{v,d}}\right)^2 + \left(\frac{F_{lat,d}}{R_{lat,d}}\right)^2 + \left(\frac{F_{ax,d}}{R_{ax,d}}\right)^2 \leq 1$$

STRUCTURAL VALUES | F_v

TIMBER-TO-TIMBER

- Characteristic values comply with the EN 1995-1-1 standard in accordance with ETA-09/0361.
- Design values can be obtained from characteristic values as follows:

$$R_d = \frac{R_k \cdot k_{mod}}{\gamma_M}$$

- In some cases the connection shear strength $R_{v,k}$ is notably large and may be higher than the secondary beam strength. Particular attention should be paid to the shear check of the reduced timber cross-section in correspondence with the bracket location.

STRUCTURAL VALUES | F_{lat} | F_{ax}

TIMBER-TO-TIMBER

- Characteristic values comply with the EN 1995-1-1 standard in accordance with ETA-09/0361. Design values can be obtained from characteristic values as follows:

$$R_{lat,d} = \min \left\{ \begin{array}{l} \frac{R_{lat,k,alu}}{\gamma_{M,alu}} \\ \frac{R_{lat,k,beam} \cdot k_{mod}}{\gamma_{M,T}} \end{array} \right.$$

$$R_{ax,d} = \frac{R_{ax,k} \cdot k_{mod}}{\gamma_M}$$

with $\gamma_{M,T}$ partial coefficient of the timber.

STRUCTURAL VALUES | F_v

TIMBER-TO-CONCRETE

- Characteristic values on wood side are consistent with EN 1995-1-1 and in accordance with ETA-09/0361. The design values of the anchors for concrete are calculated in accordance with the respective European Technical Assessments.
- Design resistance values can be obtained from the tabled values as follows:

$$R_d = \min \left\{ \begin{array}{l} \frac{R_{k, \text{timber}} \cdot k_{mod}}{\gamma_M} \\ R_{d, \text{concrete}} \end{array} \right.$$